TOWN OF GREEN MOUNTAIN FALLS PLANNING COMMISSION MEETING Tuesday, Oct 9, 2018- 6:30 PM at Town Hall

AGENDA

- 1. CALLTO ORDER/ROLL CALL, welcome guests
- 2. ADDITIONS, DELETIONS, CORRECTIONS TO THE AGENDA
- 3. APPROVE MINUTES of Sep 25, 2018
- 4. PUBLIC INPUT- For any items not on the Agenda
- 5. NEW BUSINESS
 - a. 11150 Belvidere Deck Replacement- Gregory Williamson-Contractor ACC Home Improvement
- 6. OLD BUSINESS
 - a. New FIRE STATION- Gary Florence Review Grading Plan, Drainage Report, Erosion Control Plan, Final Plat
 - b. 2019 CAPITAL IMPROVEMENTS PROGRAM (CIP) Prioritize Projects for 2019 Town Budget consideration
 - c. Frequently Asked Questions (FAQ) for Town Website GMF Submittal requirements for Building Permits and other Permits (Cactus)
 - d. GMF COMPREHENSIVE PLAN Megan Moore, Logan Simpson Company
 - 1. Overall Process and Schedule
 - 2. Preliminary Vision and Supporting Themes
 - 3. Preliminary Conditions Assessment by Theme
 - 4. Citizen Survey- Coordination and Logistics
 - 5. Next Steps
- 7. ADJOURN

TOWN OF GREEN MOUNTAIN FALLS PLANNING COMMISSION MEETING Tuesday, September 25, 2018 – 6:30 P.M.

MEETING MINUTES

PC Members Present

PC Members Absent Commissioner Gerald Irwin

Vice Chairman Dick Bratton Commissioner Greg Williamson Commissioner Rocco Blasi Chairman Eric Caldwell

Board of Trustees Members Mayor Jane Newberry

Secretary Katharine Guthrie

1. Call to Order/Roll Call

Chairman Eric Caldwell called the meeting to order at 6:36 pm.

 Additions, Deletions, or Corrections to the Agenda M/S: Caldwell/Williamson Motion: Move to accept the agenda as submitted. Vote: Motion carried. All yea.

3. Approve Minutes of September 11, 2018

M/S: Bratton/Caldwell Motion: Move to approve the minutes as submitted. Vote: Motion carried. All yea.

4. Public Input None

5. New Business

- A. Review draft 2018-2024 Capital Improvements Plan (CIP) Projects for 2019 need to be reviewed and prioritized and added to agenda for next meeting of the Planning Commission (10/9/2018)
- B. Frequently Asked Questions (FAQ) for Town website and staff—Building Permits Include: List of projects that do not require a permit
 - Clarification of permitting process (perhaps a flow chart)
 - What projects require a plan review and the process to obtain a plan review Chairman Caldwell volunteered to work on this project.

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5. Old Business

A. 10565 Foster—Cabin Renovation, Bob Vanmaarth, Contractor. Request to place a new septic system on Town Property (Flagpole Park) Tabled from meeting on 9/11/18.
 M/S: Bratton/Caldwell
 Motion: Move that we deny the request for a revocable permit on town property.
 Vote: Motion carries.

Resolution: Contractor was able to place the new septic system on his own property so there is no need to place it on town property.

- B. GMF Comprehensive Plan
 - Progress Report—GMF Project Manager Marshal is not to enforce Building Permits. Marshal is authorized to enforce municipal codes specific to GMF. Unpermitted work needs to be reported to Regional Building. Regional Building also enforces contractors licensing. GMF Business Licenses is a joint responsibility of Town Clerk working with the Marshal.
 - 2. Next Steps

2007 Plan Audit—Logan Simpson to do an analysis of the 2007 Comprehensive Plan and how it operates today.

Citizen Survey—Online, Paper, and to be added to GMF facebook page Logan Simpson is drafting the Overall Vision and will create a second Citizen Survey around the Vision

Joint Town Meeting #2—Visioning (to be scheduled)

6. Correspondence

None

Adjourned: 7:34

Eric Caldwell-Chairman

ATTEST:

Katharine Guthrie-Secretary





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REVISIONS

1. 75% CD SET 30 AUG 2018 2. 90% BID SET 30 SEP 2018

DRAWN BY: H.A CHECK BY: T.E.F

BOUNDARY SURVEY & TOPO PLAN







	ESTIMATE	ED	
1	estimated Cut	7651	Cu.Ya
2	estimated fill	4400	Cu.Ya
3	ESTIMATED EXPORT	3251	Cu.Ya
4	ESTIMATED TOP SOIL TO STOCKPILE	250	Cu.Ya

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DRAWINGS

BID

80%







F & D International, LLC Architecture . Engineering Project Management 1930 CENTRAL AVE. SUITE B BOULDER, COLORADO 80302 T : 303.652.3200 WWW. fdi-one.com





90% BID DRAWINGS





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### **MAINTENANCE & FINAL STABILIZATION:**

- 1. INSPECTION & MAINTENANCE: THE EROSION CONTROL MEASURES SHALL BE OBSERVED DAILY DURING CONSTRUCTION BY THE IDENTIFIED ADMINISTER AND AFTER EACH RAIN EVENT, HEAVY PRECIPITATION EVENT, I.E., SNOW THAT RESULTS IN RUNOFF, OR ANY QUICK SNOW MELT RUNOFF EVENT. ALL INSPECTIONS ARE TO BE DOCUMENTED IN A WRITTEN LOG AND SHALL INCLUDE (AS A MINIMUM) THE DATE OF INSPECTION, ANY INCIDENCES OF NON-COMPLIANCE, SIGNED CERTIFICATION THAT THE SITE IS IN COMPLIANCE WITH THE SWMP, AND ANY NOTES, DRAWINGS, MAPS, ETC. PERTAINING TO REPAIRS. COPIES OF ALL DOCUMENTATION SHALL BE DISTRIBUTED TO OWNER (AND OTHER AUTHORITIES HAVING JURISDICTION UPON REQUEST) ON A REGULAR BASIS AND AT A MINIMUM OF SEVEN (7) DAY INTERVALS.
- SLIT FENCING SHALL BE CHECKED FOR UNDERMINING AND BYPASS AND REPAIRED OR EXPANDED AS NEEDED. SEDIMENT SHALL BE REMOVED FROM INLET FILTERS AND SILT FENCING BEFORE ONE-HALF OF THE DESIGN DEPTH
- HAS BEEN REACHED.
- SEDIMENT IN THE PUBLIC RIGHT-OF-WAY SHALL BE REMOVED IMMEDIATELY. TEMPORARY VEGETATION OR BARE SOIL AREAS SHALL BE CHECKED REGULARLY AND SAID AREAS THAT ARE
- DAMAGED OR LOST SHALL BE RESEEDED.
- ONCE STABILIZATION HAS OCCURRED, THE CONTRACTOR IS RESPONSIBLE FOR AND SHALL INSPECT ALL BMPS EVERY
- FOURTEEN (14) DAYS AT A MINIMUM AND AFTER SIGNIFICANT PRECIPITATION OR SNOWMELT EVENTS. INSTALLATIONS AND MODIFICATIONS AS REQUIRED BY THE COMMUNITY WILL BE IMPLEMENTED WITHIN 48 HOURS OF NOTIFICATION.
- 8. CONTRACTOR SHALL REMOVE TEMPORARY EROSION CONTROL MEASURES AND REPAIR AREAS AS REQUIRED AFTER VEGETATION IS ESTABLISHED AND ACCEPTED BY OWNER AND CITY. 9. FINAL STABILIZATION AND LONG-TERM STORM WATER QUALITY: FINAL STABILIZATION IS DEFINED WHEN ALL SOIL DISTURBED AREAS AND ACTIVITIES AT THE SITE HAVE BEEN COMPLETED, AND UNIFORM VEGETATIVE COVER HAVE BEEN ESTABLISHED WITH THE DENSITY OF AT LEAST 70% OF THE PRE-DISTURBANCE LEVELS OR EQUIVALENT
- PERMANENT, AND PHYSICAL EROSION METHODS HAVE BEEN EMPLOYED. FINAL STABILIZATION WILL BE ACHIEVED USING NATIVE SEEDING, SOD, PERMANENT BMPS, AND OTHER METHODS. THE CONTRACTOR SHALL BE RESPONSIBLE FOR FINAL STABILIZATION REGARDLESS OF ACCEPTANCE BY OWNER OF THE CONTRACTOR ITEMS.

#### STRUCTURAL BMP'S:

- VEHICLE TRACKING CONTROL ("VTC"): A STABILIZED CONSTRUCTION ENTRANCE WILL BE PROVIDED AT THE ENTRANCE TO THE SITE AS CONSTRUCTION ACTIVITIES PROGRESS. THE CONSTRUCTION ACCESS AND PARKING WILL BE GRADED AND COVERED WITH CRUSHED STONE BASE COURSE DURING CONSTRUCTION. THE VTC WILL BE RELOCATED AS NEEDED TO FACILITATE CONSTRUCTION. ROUTINE INSPECTION AND MAINTENANCE WILL BE REQUIRED TO AID IN THE EFFECTIVENESS OF THE BMP AND LIMIT OFF-SITE MIGRATION OF SEDIMENT.
- SILT FENCING ("SF"): SILT FENCING SHALL BE INSTALLED WITH RESPECT TO PROPOSED DRAINAGE PATTERNS. SF SHALL BE CONSTRUCTED ALONG THE PORTIONS OF THE SITE AS SHOWN ON THE PLAN ON THE DOWNHILL PORTIONS OF THE SITE AND ALONG ANY DRAINAGE AREAS SUBJECT (OR POTENTIALLY SUBJECT) TO EROSION. THE SF SHALL BE INSTALLED AT THE DOWNHILL SIDE OF ALL EXISTING SLOPES ACROSS THE SITE AND AT ALL POINT DISCHARGE AREAS WHETHER SHOWN OF NOT. SF MUST AND SHALL BE INSPECTED AND MAINTAINED PER REGULATIONS AND AS NEEDED THROUGHOUT THE CONSTRUCTION PROCESS TO AID WITH THE EFFECTIVENESS OF THIS BMP AND LIMIT THE PROPENSITY OF OFF-SITE SEDIMENT MIGRATION. COLLECTED SEDIMENT SHALL BE REMOVED AS REQUIRED TO ENSURE THE INTEGRITY OF THE BMP. THE TEMPORARY SF SHALL REMAIN IN PLACE WITH REQUIRED INSPECTION AND MAINTENANCE THEREOF UNTIL THE STORM WATER STRUCTURES ARE COMPLETE AND THE AREA HAS BE STABILIZED BY EVIDENT OF VEGETATIVE GROUND COVER BEING ESTABLISHED. THE CONTRACTOR IS TO PROVIDE ADDITION SF AS NEEDED AND WITHOUT COST TO THE OWNER TO MAINTAIN THE BASIS OF INTENT OF THE SF WHETHER OR NOT IT IS SHOWN ON THE DRAWINGS.
- C. INLET PROTECTION ("IP"): THE INLET PROTECTION WILL BE INSTALLED AS THE STORM SEWER STRUCTURES ARE CONSTRUCTED. EACH INLET ON THE PROPOSED STORM SEWER SYSTEM WILL HAVE A TEMPORARY INLET SEDIMENT TRAP CONSTRUCTED IN SUCH A MANNER THAT IS CIRCUMSCRIBES THE INLET. IN PAVED AND NON-PAVED AREAS, INCLUDING GRAVEL IMPROVED AREAS, THIS TRAP IS TO CONSIST OF WIRE MESH ROCK SOCKS TO ACT AS A FILTER OF STORM WATER RUNOFF AND TO ALLOW ANY SILT TO SETTLE OUT. IP PROTECTION SHALL AND MUST BE INSPECTED AND MAINTAINED PER REGULATIONS AND AS NEEDED FOR THE DURATION OF THE CONSTRUCTION PROCESS TO AID WITH THE EFFECTIVENESS OF THIS BMP AND TO LIMIT THE PROPENSITY OF OFF-SITE SEDIMENT MIGRATION. ALL COLLECTED SEDIMENT SHALL BE PROPERLY REMOVED AS REQUIRED BY THE CONTRACTOR.
- OUTLET PROTECTION ("OP"): THE STORM SEWER OUTLETS SHALL BE PROTECTED WITH RIPRAP. PLACING RIPRAP AT PIPE OUTFALLS REDUCE IS DESIGNED TO REDUCE THE EXIT VELOCITY AND REDUCE SOURING EFFECTS OF THE STORM WATER DISCHARGE. THE RIPRAP SHALL BE LEFT IN PLACE AS PART OF THE PERMANENT STORM WATER MANAGEMENT AND STABILIZATION PLAN.
- OVER LOT GRADING MEASURES ("OGM"): ALL OPEN AREAS INCLUDING STOCKPILES SHALL BE TREATED WITHIN URTEEN (14) DAYS OF COMPLETION OF OVER-LOT GRADING. ALL OVER-LOT GRADING IN THE NON-IRRIGATED AREAS SHALL HAVE THE SURFACE ROUGHENED AND SHALL BE PERMANENTLY LANDSCAPED OR TEMPORARY SEEDED UNTIL THE PLANED FINAL INSTALLATIONS ARE COMPLETED. AT THE COMPLETION OF THE MASS GRADING, ALL EXPOSED SOIL AREAS SHALL HAVE THE SURFACE ROUGHENED AND PLANTED WITH A RE-VEGETATION SEED MIX APPROPRIATE FOR THE AREA OR A MIX AS DIRECTED BY THE COUNTY OR CITY. VEGETATION IS TO BE MAINTAINED THROUGH THE CONSTRUCTION PERIOD AND UNTIL SAID VEGETATION BECOMES ESTABLISHED BY THE CONTRACTOR AT THE CONTRACTOR'S EXPENSE, THIS MAY INCLUDE, BUT NOT LIMITED TO RE-SEEDING AS REQUIRED TO ENSURE ADEQUATE RE-VEGETATION DENSITY, MAINTAINING AND CLEANING UP ANY EROSION ISSUES, ETC. AREAS THAT WILL RECEIVE FINAL LANDSCAPING, THE CONTRACTOR ONLY NEEDS TO MAINTAIN UNTIL FINAL LANDSCAPING IS INSTALLED. ALTERNATIVELY, ROUGH-CUT DRIVEWAYS OR PROPOSED PAVED AREAS ARE TO BE COVERED WITH A LAYER OF AGGREGATE, ROAD BASE OR ASPHALT PAVING.
- DUST CONTROL MEASURES ("DCM"): ALL DISTURBED AREAS (REGARDLESS AS TO THE LIMITS OF SAID DISTURBED AREA) THAT ARE NOT YET READY TO BE SEEDED, LANDSCAPED, PAVED, OR OTHERWISE STABILIZED SHALL BE WATERED, OR RIPPED AS NECESSARY TO PRECLUDE VISIBLE DUST EMISSIONS.
- G. PHASE MEASURES ("PM"): PM'S ARE DEFINED AS ITEMS THAT ARE SCHEDULED TO BE IMPLEMENTED ACCORDING TO HE CONSTRUCTION SCHEDULE. AS WORK PROGRESS, IMPLEMENTATION OF INDIVIDUAL BMPS IS TO COINCIDE WITH THE CONSTRUCTION AND ORCHESTRATED AS APPROPRIATE TO ENSURE PROPER IMPLEMENTATION OF BMPS, THEREBY MINIMIZING THE EXPOSURE OF UNPROTECTED AREAS. SF, IP (EXISTING INLETS), AND GRAVELING OF THE CONSTRUCTION ENTRANCE SHALL BE PERFORMED PRIOR TO THE START OF ANY GRADING. ADDITIONAL IP WILL BE INSTALLED AS THE STORM SEWER STRUCTURES ARE CONSTRUCTED. THE RIPRAP PROTECTION SHALL BE INSTALLED AS THE STORM SEWER OUTFALLS OR CULVERTS ARE CONSTRUCTED. THE STRUCTURAL BMPS THAT DO NOT BECOME PART OF THE PERMANENT STORM WATER MANAGEMENT PLAN ARE TO BE REMOVED, AS THE PAVING, LANDSCAPING, AND OTHER PERMANENT GROUNDCOVER INSTALLATIONS ARE COMPLETED AND ESTABLISHED. WITH RESPECT TO OVER-LOT SEEDING, ESTABLISHMENT OF SUCH RE-VEGETATION MAY BE 12 MONTHS OF LONGER. FUGITIVE DUST EMISSIONS RESULTING FROM GRADING ACTIVITIES AND/OR WIND SHALL BE CONTROLLED USING THE BEST AVAILABLE CONTROL TECHNOLOGY AS DEFINED BY THE CDPHE AT THE TIME OF GRADING. THE GRAVELING IS TO BE MAINTAINED AND EXTENDED CONSTRUCTION PROGRESSES ESPECIALLY AROUND THE BUILDING SITE. THE STRUCTURAL BMPS ARE TO BE REMOVED, AS THE PERMANENT LANDSCAPING INSTALLATIONS ARE COMPLETED. NOTE THE EROSION AND SEDIMENT CONTROL PLAN MAY BE MODIFIED BY THE CONTRACTOR OR OWNER'S ENGINEER OR ITS AUTHORIZED REPRESENTATIVE AS FIELD CONDITIONS WARRANT.
- H. SEEDING & MULCHING: ALL SEEDS FURNISHED SHALL BE FREE FROM NOXIOUS SEEDS SUCH AS RUSSIAN OR CANADIAN THISTLE, COURSE FESCUE, EUROPEAN BINDWEED, JOHNSON GRASS, KNAPWEED, LEAFY SURGE, OTHER SPECIES AS DEFINED BY THE LOCAL JURISDICTION. REFER TO COLORADO'S WEED LIST WEBSITE AT WWW.CWMA.ORG/NXWDID.HTM. THE SEED MUST BE FRESH, WITHOUT MOLD, AND OF HIGH QUALITY. THE COUNTY OR CITY MAY HAVE A PREFERRED SEED MIX, IN WHICH CASE THAT MIX SHALL BE USED WITHOUT EXCEPTIONS TO THE NEED TO ENSURE THE MIX IS VOID OF IDENTIFIED NOXIOUS WEEDS AS NOTED ABOVE. THE FORMULA USED TO DETERMINE THE QUALITY OF THE PURE LIVE SEED ("PLS") SHALL BE "(POUNDS OF SEED) X (PURITY) X (GERMINATION) = POUNDS OF PURE LIVE SEED OR PLS". SEEDING RECOMMENDATIONS ARE AS NOTED, BUT MAY BE MODIFIED WITH THE OWNER'S APPROVAL TO MAKE THE BEST USE OF EXISTING CLEARINGS AND GRUBBINGS. ALL SEEDS SHALL BE DRILLED, BROADCASTED OR HYDRO-SEEDED. ALL DISTURBED AREAS SHALL BE SEEDED AND MULCHED IF PERMANENT VEGETATION IS NOT IMMEDIATELY INSTALLED. AFTER SEEDING HAS BEEN COMPLETED, STRAW AT A RATE OF 4,000 LB PER ACRE SHALL BE APPLIED UNIFORMLY (CLEAN STRAW), CRIMPED IN WITH A CRIMPER OR OTHER APPROVED EQUIPMENT OR OTHERWISE ATTACHED. A HYDRAULICALLY APPLIED TRACIFER OR NETTING TO ATTACH MULCH, PER MANUFACTURER'S INSTALLATION INSTRUCTIONS, MAY BE USED WITH THE OWNER'S APPROVAL. THE SEEDED AREA SHALL BE CRIMPED MULCHED AND THE MULCH ATTACHED WITHIN TWENTY-FOUR (24) HOURS AFTER SEEDING. AREAS NOT MULCHED AND ATTACHED WITHIN THE DEFINED TWENTY-FOUR (24) HOUR AFTER SEEDING SHALL BE RE-SEEDED WITH THE SPECIFIED MIX AT THE CONTRACTOR'S EXPENSE, PRIOR TO MULCHING AND ATTACHING. ON STEEP SLOPES OR OTHER SPECIFIED AREAS AS SHOWN HEREIN, WHICH ARE DESIGNATED AS AREAS, PER THE OWNER'S ENGINEER, AS DIFFICULT TO MULCH AND ATTACH BY CONVENTIONAL METHODS; BURLAP OR OTHER BLANKETING MATERIALS SHALL BE USED AND PROPERLY ANCHORED AND SECURED. AREAS STEEPER THEN
- ¹/₃ SHALL BE PROTECTED WITH APPROVED RECP. PERMANENT STABILIZATION MEASURES ("PSM"): RIPRAP FOR STORM DRAIN OUTFALLS AND ROCK CHECK DAMS SHALL BECOME PART OF THE PERMANENT STORM WATER MANAGEMENT PLAN AND WILL NOT BE REMOVED. PERMANENT LANDSCAPING WILL INCLUDE BUT NOT LIMITED TO; SEEDING, INSTALLATION OF SOD OR OTHER VEGETATION COVER TO OPEN AREAS AS SHOWN. NATIVE PERENNIAL SEEDING SHALL BE ESTABLISHED IN NON-IRRIGATED AREAS AND OTHER VEGETATIVE COVER SHALL BE ESTABLISHED IN IRRIGATED OPEN AREAS (IF ANY). ALL PERMANENT STABILIZATION MEASURES WILL BE SPECIFIED HEREIN.

#### STORM WATER MANAGEMENT CONTROLS:

## STORM WATER MANAGEMENT PLAN (SWMP)

NAME: TITLE: CONTACT INFO: _____

PHASE SITE RESTORATION

4. OTHER POTENTIAL POLLUTION SOURCES SUCH AS VEHICLE FUELING, STORAGE, FERTILIZERS OR CHEMICALS, VEHICLE WASHING, WASTE DISPOSAL, HAUL-ROADS, LOADING AND UNLOADING AREAS, MASONRY AND CONCRETE WASHOUT, ETC. ARE LOCATED WITHIN THE STABILIZED CONSTRUCTION AREAS AS SHOWN ON THE PLANS. IF CONSTRUCTION DEWATERING OCCURS ON SITE, A SEPARATE GROUND WATER DISCHARGE PERMIT WILL BE REQUIRED AND ADHERED TO.

1. NON STRUCTURAL BMPS WILL BE IMPLEMENTED TO THE MAXIMUM EXTENT POSSIBLE. THE UTILIZATION OF NON-STRUCTURAL BMPS WILL BE AN ONGOING PROCESS DIRECTED AT PREVENTING EROSION. THE NON-STRUCTURAL BMPS WILL RECEIVE CONTINUOUS EMPHASIS THROUGHOUT THE CONSTRUCTION PROCESS BECAUSE SAID BMPS WILL AVERT PROBLEMS BEFORE THEY OCCUR AND REDUCE THE PROPENSITY FOR STRUCTURAL BMPS. NON-STRUCTURAL BMPS WILL CONSIST PRIMARILY OF THE PRESERVATION OF EXISTING MATURE VEGETATION AND TREES, PLANNING, AND SCHEDULING OF CONSTRUCTION ACTIVITIES AIMED AT ACHIEVING A GOAL OF MINIMIZING EROSION. FURTHERMORE, CONSTRUCTION PERSONNEL WILL BE INSTRUCTED AND SUPERVISED IN CONSTRUCTION METHODS CONSISTENT WITH EROSION PREVENTION PRACTICES.

2. PLANNED STRUCTURAL BMPS FOR EROSION AND SEDIMENT CONTROL ARE SHOWN ON THE EROSION AND SEDIMENTATION CONTROL PLAN. IMPLEMENTING THESE METHODS SHOULD MINIMIZE NUISANCE SILT AND SEDIMENTATION EXITING THE SITE AND PREVENT CLOGGING EXISTING DOWNSTREAM STORM WATER CONVEYANCE SYSTEMS.

3. APPLICATION OF THESE BMPS FOR STORM WATER MANAGEMENT IS FOR THE CONSTRUCTION PERIODS AND IS CONSIDERED TEMPORARY IN NATURE. POST-DEVELOPMENT STORM WATER MANAGEMENT IS PROVIDED THROUGH VEGETATED LANDSCAPED AREAS, GRASSED SWALES, RIPRAP PROTECTION AND THE STORM WATER COLLECTION SYSTEM.

4. OTHER POTENTIAL POLLUTION SOURCES SUCH AS VEHICLE FUELING, STORAGE, FERTILIZERS OR CHEMICALS, VEHICLE WASHING, WASTE DISPOSAL, HAUL-ROADS, LOADING AND UNLOADING AREAS, MASONRY AND CONCRETE WASHOUT, ETC. ARE LOCATED WITHIN THE STABILIZED CONSTRUCTION AREAS AS SHOWN ON THE PLANS. NON-STORM WATER COMPONENTS OF THE DISCHARGE, SUCH AS SPRINGS MAY BE FOUND ON THE SITE. IF CONSTRUCTION DEWATERING OCCURS ON SITE, A SEPARATE GROUND WATER DISCHARGE PERMIT WILL BE REQUIRED AND ADHERED TO.

5. SIGNIFICANT OFF-SITE RUNOFF FLOWS ARE NOT ANTICIPATED WITH THIS PROJECT. HISTORIC ON-SITE FLOWS ARE GENERALLY CONVEYED TO THE SOUTH AND TO THE EAST. DEVELOPED ON-SITE FLOWS WILL BE CONTAINED WITHIN THE PROPOSED STORM WATER NETWORK FOR CONVEYANCE TO THE ONSITE DETENTION AND WATER QUALITY FACILITIES. STORM WATER IS DISCHARGED FROM THIS SITE TO THE NATURAL MAJOR DRAINAGE WAY WITH THE ULTIMATE OUTFALL TO THE NORTH SAINT CHARLES RIVER.

#### GENERAL REQUIREMENTS:

1. THE STORM WATER MANAGEMENT PLANT IS TO BE RETAINED AND MAINTAINED ON-SITE ALONG WITH ANY OTHER EROSION CONTROL DOCUMENTATION INCLUDING BUT NOT LIMITED TO UPDATED PLANS, MAINTENANCE RECORDS, AND REPORTS ALONG WITH THE REFERENCED LANDSCAPE PLAN. A SWMP ADMINISTRATOR WILL BE DESIGNATED BY THE CONTRACTOR AND IS RESPONSIBLE FOR DEVELOPING, IMPLEMENTING, MAINTAINING, AND REVISING THE SWMP. THE SWMP ADMINISTRATOR IS THE CONTACT FOR ALL SWMP-RELATED ISSUES AND IS RESPONSIBLE FOR ITS ACCURACY, COMPLETENESS, AND IMPLEMENTATION. THE FOLLOWING PERSON HAS BEEN DESIGNATED AS THE SWMP ADMINISTRATOR FOR THIS PROJECT:

2. GREEN MOUNTAIN/CHIPITA PARK FIRE PROTECTION DISTRICT ADMINISTRATIVE AND STORAGE FACILITY, THE "PROJECT" IS LOCATED WITHIN THE COMMUNITY OF GREEN MOUNTAIN FALLS, COLORADO, AT APPROXIMATELY LATITUDE AND LONGITUDE. THE PROJECT GENERALLY CONSISTS OF SITE GRADING, LINEAR IMPROVEMENTS FOR A WATER SERVICE, ROAD IMPROVEMENTS SEPTIC SYSTEM, STORM WATER SEWER, STORM DRAINAGE SYSTEM, CONSTRUCTION OF AN ACCESS DRIVEWAY, AND CONSTRUCTION OF A FIRE STATION. THE ANTICIPATED DISTURBED AREA IS ESTIMATED AT APPROXIMATELY 2 ACRES. THE TOTAL SITE AREA IS 2 ACRES. NO AREA GREATER THAN 40 ACRES SHALL BE DISTURBED AT ANY GIVEN TIME. NO CONSTRUCTION ACTIVITIES SHALL OCCUR OFF-SITE OR OUTSIDE OF THE CONSTRUCTION LIMITS SHOWN ON THE PLANS. THE ESTIMATED SEQUENCE OF CONSTRUCTION IS AS FOLLOWS:

estimated ACTUAL CONSTRUCTION START

3. THE PRESENT SITE CONSISTS OF THE UNDEVELOPED LAND AND IS APPROXIMATELY 90% COVERED WITH VEGETATIVE GROUND COVER, I.E., NATIVE GRASSES. EXISTING SOIL CONSISTS OF SOIL TYPE(S) CL, SC, SP-SC AND CH ACCORDING TO NRCS STANDARDS. THE ESTIMATED HISTORICAL AND DEVELOPED 100 YEAR RUNOFF COEFFICIENTS ARE NOT EXPECTED TO BE SIGNIFICANTLY ALTERED WITH THIS PROJECT. SEE SUBSURFACE GEOTECH REPORT.

5. SIGNIFICANT OFF-SITE RUNOFF FLOWS ARE NOT ANTICIPATED WITH THIS PROJECT. HISTORIC ON-SITE FLOWS ARE GENERALLY CONVEYED TO THE WEST AND SOUTH AND TO THE EAST AND SOUTH. DEVELOPED ON-SITE FLOWS WILL BE CONTAINED WITHIN THE PROPOSED STORM WATER NETWORK FOR CONVEYANCE TO THE ONSITE DETENTION AND WATER QUALITY FACILITIES.

1. THE CONTRACTOR SHALL CLEAR AND GRUB THE PROPOSED AREA OF DISTURBANCE PRIOR TO EXCAVATION. THE PROPOSED AREA OF DISTURBANCE IS APPROXIMATELY 2 ACRES. 2. THE SITE GENERALLY CONSISTS OF 2 TO 4 INCHES OF TOPSOIL, THE CONTRACTOR SHALL REMOVE AND

STOCKPILE EXISTING TOPSOIL FOR USE WITH NATIVE SEEDING OPERATIONS. APPROXIMATELY 1,950CY OF TOPSOIL EXISTS ONSITE

3. CONTACT THE ENGINEER FOR THE GEOTECHNICAL SUBSURFACE REPORT

4. SEEDING SHALL CONFORM TO THE LATEST EDITION OF THE DENVER URBAN DRAINAGE DESIGN MANUAL. NATIVE SEED MIX SHALL SATISFY EL PAYO COUNTY AND/OR REGIONAL REQUIREMENTS 5. SURFACE ROUGHING SHALL BE PROVIDED PROMPTLY AFTER COMPLETION OF FINISH GRADE, PRIOR TO

SEEDING, PRIOR TO RAIN EVENTS AND AS DIRECTED BY THE ENGINEER . NO WORK ON COMMENCE IN PUBLIC R.O.W WITH SECURING ALL LOCAL, REGIONAL PERMITS.

7. INSTALL SEDIMENT LOGS IN ALL EXISTING NATURAL DRAINAGE SWALES THAT ARE IMPACTED OR COULD BE IMPACTED BY CONSTRUCTION EFFECTS.

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MING RA  $\square$ BID 80%

![](_page_12_Picture_0.jpeg)

![](_page_13_Figure_0.jpeg)

![](_page_13_Picture_1.jpeg)

![](_page_14_Figure_0.jpeg)

![](_page_14_Figure_1.jpeg)

NOTES: 1. LOCATE EROSION LOGS AT THE OUTSIDE EDGE OF THE CONCRETE APRON

# DROP INLET PROTECTION DETAIL N.T.S.

# **Rolled Erosion Control Products (RECP)**

- -TYPE OF ECB (STRAW, STRAW-COCONUT, COCONUT, OR EXCELSIOR). -AREA, A, IN SQUARE YARDS OF EACH TYPE OF ECB.
- 2. 100% NATURAL AND BIODEGRADABLE MATERIALS ARE PREFERRED FOR RECPS, ALTHOUGH SOME JURISDICTIONS MAY ALLOW OTHER MATERIALS IN SOME APPLICATIONS.

3. IN AREAS WHERE ECBs ARE SHOWN ON THE PLANS, THE PERMITTEE SHALL PLACE TOPSOIL AND PERFORM FINAL GRADING, SURFACE PREPARATION, AND SEEDING AND MULCHING. SUBGRADE SHALL BE SMOOTH AND MOIST PRIOR TO ECB INSTALLATION AND THE ECB SHALL BE IN FULL CONTACT WITH SUBGRADE. NO GAPS OR VOIDS SHALL EXIST UNDER THE

4. PERIMETER ANCHOR TRENCH SHALL BE USED ALONG THE OUTSIDE PERIMETER OF ALL

5. JOINT ANCHOR TRENCH SHALL BE USED TO JOIN ROLLS OF ECBs TOGETHER (LONGITUDINALLY AND TRANSVERSELY) FOR ALL ECBs EXCEPT STRAW WHICH MAY USE

6. INTERMEDIATE ANCHOR TRENCH SHALL BE USED AT SPACING OF ONE-HALF ROLL LENGTH

FOR COCONUT AND EXCELSIOR ECBs. 7. OVERLAPPING JOINT DETAIL SHALL BE USED TO JOIN ROLLS OF ECBs TOGETHER FOR ECBs

8. MATERIAL SPECIFICATIONS OF ECBs SHALL CONFORM TO TABLE ECB-1.

9. ANY AREAS OF SEEDING AND MULCHING DISTURBED IN THE PROCESS OF INSTALLING ECBS SHALL BE RESEEDED AND MULCHED.

10. DETAILS ON DESIGN PLANS FOR MAJOR DRAINAGEWAY STABILIZATION WILL GOVERN IF DIFFERENT FROM THOSE SHOWN HERE.

TABLE ECB-1. ECB MATERIAL SPECIFICATIONS					
TYPE	COCONUT CONTENT	STRAW CONTENT	EXCELSIOR CONTENT	RECOMMENDED NETTING**	
STRAW*	_	100%	_	DOUBLE/ NATURAL	
STRAW- COCONUT	30% MIN	70% MAX	-	DOUBLE/ NATURAL	
COCONUT	100%	_	_	DOUBLE/ NATURAL	
EXCELSIOR	-	_	100%	DOUBLE/ NATURAL	

*STRAW ECBs MAY ONLY BE USED OUTSIDE OF STREAMS AND DRAINAGE CHANNEL. **ALTERNATE NETTING MAY BE ACCEPTABLE IN SOME JURISDICTIONS

Urban Drainage and Flood Control District Urban Storm Drainage Criteria Manual Volume 3 November 2010

# **Rolled Erosion Control Pr**

Flow

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EROSION CONTROL BLANKET MAINTENANCE 1. INSPECT BMPs EACH WORKDAY, AND M MAINTENANCE OF BMPs SHOULD BE PROA POSSIBLE (AND ALWAYS WITHIN 24 HOURS EROSION, AND PERFORM NECESSARY MAIN 2. FREQUENT OBSERVATIONS AND MAINTEN EFFECTIVE OPERATING CONDITION. INSPECT DOCUMENTED THOROUGHLY. 3. WHERE BMPs HAVE FAILED, REPAIR OR DISCOVERY OF THE FAILURE. 4. ECBs SHALL BE LEFT IN PLACE TO EVE REMOVED BY THE LOCAL JURISDICTION. 5. ANY ECB PULLED OUT, TORN, OR OTHE REINSTALLED. ANY SUBGRADE AREAS BELO A VOID UNDER THE BLANKET, OR THAT F RESEEDED AND MULCHED AND THE ECB NOTE: MANY JURISDICTIONS HAVE BMP DET/ CONSULT WITH LOCAL JURISDICTIONS AS TO DIFFERENCES ARE NOTED. (DETAILS ADAPTED FROM DOUGLAS COUNTY, COLORADO

November 2010

Urban Drainage and F Urban Storm Drainage Crit

FLOW INLET		<image/> <section-header><section-header><section-header><section-header><section-header><section-header><text><text></text></text></section-header></section-header></section-header></section-header></section-header></section-header>
SECTION A - A NTS		GREEN MONTAIN FALLS FIRE DISTRICT         GREEN MONTAIN FALLS FIRE DISTRICT         Fire Station Project Two Carsell Way         Green Montain Falls, El Paso County, CO         1. 75% CD SET 30 AUG 2018         1. 75% CD SET 30 AUG 2018
lood Control District RECP-9	90% BID DRAWINGS	<image/> <text><text><text><text></text></text></text></text>

![](_page_15_Figure_0.jpeg)

# Sediment Control Log (SCL)

3. SEDIMENT CONTROL LOGS SHALL CONSIST OF STRAW, COMPOST, EXCELSIOR OR COCONUT

5. IT IS RECOMMENDED THAT SEDIMENT CONTROL LOGS BE TRENCHED INTO THE GROUND TO DEPTH IS NOT FEASIBLE AND/OR DESIRABLE (SHORT TERM INSTALLATION WITH DESIRE NOT TO DAMAGE LANDSCAPE) A LESSER TRENCHING DEPTH MAY BE ACCEPTABLE WITH MORE ROBUST

6. THE UPHILL SIDE OF THE SEDIMENT CONTROL LOG SHALL BE BACKFILLED WITH SOIL OR FILTER MATERIAL THAT IS FREE OF ROCKS AND DEBRIS. THE SOIL SHALL BE TIGHTLY COMPACTED INTO THE SHAPE OF A RIGHT TRIANGLE USING A SHOVEL OR WEIGHTED LAWN

7. FOLLOW MANUFACTURERS' GUIDANCE FOR STAKING. IF MANUFACTURERS' INSTRUCTIONS MINIMUM OF 6" INTO THE GROUND. 3" OF THE STAKE SHALL PROTRUDE FROM THE TOP OF THE LOG. STAKES THAT ARE BROKEN PRIOR TO INSTALLATION SHALL BE REPLACED. COMPOST

4. SEDIMENT ACCUMULATED UPSTREAM OF SEDIMENT CONTROL LOG SHALL BE REMOVED AS NEEDED TO MAINTAIN FUNCTIONALITY OF THE BMP, TYPICALLY WHEN DEPTH OF ACCUMULATED

TOP SOIL, SEEDED AND MULCHED OR OTHERWISE STABILIZED IN A MANNER APPROVED BY

November 2015

![](_page_15_Picture_17.jpeg)

## F & D International, LLC Architecture . Engineering

Project Management 1930 CENTRAL AVE. SUITE B BOULDER, COLORADO 80302 T:303.652.3200 WWW. fdi-one.com

DISTRIC σ Ш 5 FIR <u>e</u> S ()S Δ Ш Ш +-lls Z ▼ 0 . O ш σ Z 4 atio  $\supset$ St Σ Ð 2 Ш Ш  $\sim$  $\bigcirc$ REVISIONS 1. 75% CD SET 30 AUG 2018 2. 90% BID SET 30 SEP 2018 DATE: 30-SEP-18 DRAWN BY: H.A CHECK BY: T.E.F EROSION CONTROL DETAILS C 5.4

S

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MIN

RA

 $\square$ 

BID

80%

![](_page_16_Figure_0.jpeg)

![](_page_16_Figure_1.jpeg)

SECTION A-A

## CONCRETE WASHOUT FACILITY DETAIL

<b>EC-1</b>	Surface Roughening (SR)	Sediment Control Log (
		SCL SCL
<u>s</u>	SURFACE ROUGHENING INSTALLATION NOTES	
1	. SEE PLAN VIEW FOR: -LOCATION(S) OF SURFACE ROUGHENING.	
2 G F	. SURFACE ROUGHENING SHALL BE PROVIDED PROMPTLY AFTER COMPLETION OF FINISHED RADING (FOR AREAS NOT RECEIVING TOPSOIL) OR PRIOR TO TOPSOIL PLACEMENT OR ANY ORECASTED RAIN EVENT.	
3 D	5. AREAS WHERE BUILDING FOUNDATIONS, PAVEMENT, OR SOD WILL BE PLACED WITHOUT DELAY IN THE CONSTRUCTION SEQUENCE, SURFACE ROUGHENING IS NOT REQUIRED.	ON CENTER (TYP
4 TI	. DISTURBED SURFACES SHALL BE ROUGHENED USING RIPPING OR TILLING EQUIPMENT ON HE CONTOUR OR TRACKING UP AND DOWN A SLOPE USING EQUIPMENT TREADS.	FLOW OF SCL
5	. A FARMING DISK SHALL NOT BE USED FOR SURFACE ROUGHENING.	
<u>s</u>	URFACE ROUGHENING MAINTENANCE NOTES	
1. M P E	. INSPECT BMPs EACH WORKDAY, AND MAINTAIN THEM IN EFFECTIVE OPERATING CONDITION. IAINTENANCE OF BMPs SHOULD BE PROACTIVE, NOT REACTIVE. INSPECT BMPs AS SOON AS POSSIBLE (AND ALWAYS WITHIN 24 HOURS) FOLLOWING A STORM THAT CAUSES SURFACE ROSION, AND PERFORM NECESSARY MAINTENANCE.	TRENCHED SE
2 E D	2. FREQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN BMPs IN EFFECTIVE OPERATING CONDITION. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY.	COMPACTED EXCAVATED
3	. WHERE BMPS HAVE FAILED, REPAIR OR REPLACE UPON DISCOVERY OF THE FAILURE.	TRENCH SOIL
4 R	. VEHICLES AND EQUIPMENT SHALL NOT BE DRIVEN OVER AREAS THAT HAVE BEEN SURFACE COUGHENED.	FLOW
5 D	. IN NON-TURF GRASS FINISHED AREAS, SEEDING AND MULCHING SHALL TAKE PLACE PIRECTLY OVER SURFACE ROUGHENED AREAS WITHOUT FIRST SMOOTHING OUT THE SURFACE.	
6 R E	G. IN AREAS NOT SEEDED AND MULCHED AFTER SURFACE ROUGHENING, SURFACES SHALL BE RE—ROUGHENED AS NECESSARY TO MAINTAIN GROOVE DEPTH AND SMOOTH OVER RILL ROSION.	
(0	DETAILS ADAPTED FROM TOWN OF PARKER, COLORADO, NOT AVAILABLE IN AUTOCAD)	TRENCHED SEDIM
	IOTE: MANY JURISDICTIONS HAVE BMP DETAILS THAT VARY FROM UDFCD STANDARD DETAILS. CONSULT WITH LOCAL JURISDICTIONS AS TO WHICH DETAIL SHOULD BE USED WHEN DIFFERENCES ARE NOTED.	12" OVERIA
		(MIN.)
		9" DIAMETER (MIN)
		SCL-1. TRENCHED
SR-4	Urban Drainage and Flood Control DistrictNovember 2010Urban Storm Drainage Criteria Manual Volume 3	November 2015 Urban Drainage an Urban Storm Drainage

![](_page_16_Figure_5.jpeg)

### **DRAINAGE REPORT FOR**

# GREEN MOUNTAIN FALLS / CHIPITA PARK FIRE PROTECTION DISTRICT

### **CENTRAL FIRE STATION**

## Two Carsell Way, Green mountain Falls, Colorado 80819 30 August 2018

Prepared By:

F&D International LLC 1930 Central Ave., Unit #B Boulder, CO 80301 (P) 303.652.3200 F&D Project No. 15004

![](_page_17_Picture_6.jpeg)

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Existing Conditions	Page 1
Proposed Developed Drainage Plan	Page 1
Conclusions	Page 4
References	Page 5
Appendix A – Vicinity Map	Page A1
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Appendix C – Details	Page C1

![](_page_18_Picture_4.jpeg)

#### INTRODUCTION

#### GENERAL LOCATION AND DESCRIPTION

The Green Mountain Falls / Chipita Park Fire Protection District (District) proposes to construct a new central response fire station (Station) at Two Carsell Way, Green Mountain Falls, Colorado. The site is located within part of the Northwest ¹/₄, Northeast 1/4 of Section 8, Township 12 South, Range 68 West, 6th Principal Meridian, Green Mountain Falls, El Paso County, Colorado. The property is bound to the west, north, and south by developed properties and the east by US Highway 24. A vicinity map is located in Appendix A of this report.

#### PROPOSED DEVELOPMENT

The District is constructing a new central response fire station. The new facility is proposed to be approximately 14,000 ft² response fire station

#### **EXISTING CONDITIONS**

#### EXISTING DRAINAGE

Lot 2 - Lot 2 is a vacant undeveloped lot. The lot gradient primarily ranges from 25% to 5%. The western portion of the lot slopes generally to the south. The eastern half of the side slopes to the east and south.

Lot 1 - Lot 1 is a developed lot and contains a graveled surface parking lot and the Green Mountain Falls Townhall and police department. This lot has a gradient ranging from 30% to 5% and slopes generally to the south. The intention of this report is to incorporate and improve the drainage systems associated with the Lot 1 and incorporate the drainage with Lot 2.

According to FEMA Flood Insurance Rate Map for this project, both Lot 1 and Lot 2 are not located in a flood plain

#### PROPOSED (DEVELOPED) DRAINAGE

#### DRAINAGE DESIGN CRITERIA

The proposed drainage facilities have been designed to comply with the City of Colorado Springs Drainage Criteria Manual, 2014 edition. This manual has been adopted by El Paso county as their stormwater criteria manual.

#### HYDROLOGIC METHOD AND DESIGN STORM FREQUENCIES

The Rational Method (Q=CIA) was used to determine the storm runoff (Q) from the sites, with a composite runoff coefficient (C) and contributing areas (A) given for design points in sub basins. The runoff coefficients for various land uses where obtained from City of Colorado Springs Drainage Criteria Manual. Intensities (I) were determined using the Time-Intensity-Frequency Values (Figure 5, El Paso County) and a calculated Time of Concentration (tc). Post development time concentration calculations for each sub-basin, corresponding rainfall intensities, composite runoff coefficients, and storm flows for the 10-year and 100-year storms for each design point are provided in the appendix. Runoff rates have been shown on the included drainage map.

The total detention volume for this site was determined using the following equation;

 $V_{required} = ((V_{runoff} - V_{discharge}) + V_{Water Quality})*FS$ 

#### Where

V_{required} is defined as the total required detention volume

 $V_{\text{runoff}}$  is defined as the runoff volume from the site

 $V_{\mbox{\scriptsize discharge}}$  is defined as the allowable discharge volume for storm event

V_{Water Quality} is defined as the additional WQCV volume required for water quality

FS is the Factor of Safety

The historic and developed volumes where calculated from the subject properties. The Water Quality Capture Volume (WQCV) was calculated from the total lot area. The 100 year volume was calculated from the composite area of the defined on-site sub basins. It is assumed that all offsite properties that drain to the subject property will restrict developed release rates to the historic values. The offsite flows will therefore be routed un-detained through the pond. It is also assumed that the property to the west and Hwy 24 ROW to the north of the subject property will reach Fountain Creek and will not impact the proposed drainage system. Undeveloped and impacted areas of the subject properties will retain their respective historical flows.

#### SITE BASINS AND SUB-BASINS

The proposed site drainage consists of nine (9) major basins, two (2) Of-Site Basins OS and seven (7) On Site Basins A-G. Basins A-G are divided according to the areas that drain into each proposed stormwater structure on the site. This was done to simplify the calculations for sizing of swales, pipes and inlets in each basin.

Description of Major Drainage Basins

Basin "A" (13915.19 sf/ 0.319 acres) is comprised of the proposed parking and concrete apron at the south face of the proposed fire station. All drainage within Basin A sheet flows across parking area into a Type R Curb inlet along southern curb of parking

Basin "B" (11748.61 sf/ 0.270 acres) is comprised of the north eastern section of Lot 2. Drainage from this basin includes stormwater flowing from the eastern wing of the proposed building and building pad along with flows from the historic site above the eastern retaining wall. These flows are captured in a Type C inlet located at the interception of the proposed roadway and parking pad.

Basin "C" (8492.99 sf/ 0.1950acres) is comprised of the eastern half of the inner curve of the proposed roadway. Flows from this basin sheet flow across the historic site as well as the proposed roadway into a drainage swale along the roadway and is then carried to another Type C inlet at the southernmost point of the proposed roadway.

Basin "D" (7410.6971sf/ 0.170 acres) is comprised of the western half of the proposed roadway. Flows from this basin sheet flow across the historic site as well as the proposed roadway into a drainage swale along the roadway and is then carried to another Type C inlet located along the proposed roadway before the retaining wall also along the road.

Basin "E" (35250.59sf/ 0.809 acres) is comprised of the north western quarter of Lot 2. This area includes the center and western sections of the fire station and building pad, and historic flows from the existing drainage on the northern section of Lot 2. All drainage either sheet flows into the proposed Type C inlet directly or flows into a series of swales that transport the drainage into the inlet.

Basin "F" (21500.08sf/ 0.494 acres) is comprised of the north eastern section of lot 1. Flows from this basin sheet flow across the historic site into a drainage swale and then into the final Type C inlet that transports the flows into the detention basin.

Basin "G" (35865.94sf/ 0.823) is comprised of the existing town hall site located in lot 1. Flows from this basin flow directly from the town hall site and into the detention basin.

Basin "OS" (9939.16sf/0.228 acres) is comprised of a section of existing road and grading that slope off site and drain onto Green Mountain Falls Road as historical drainage that will not be captured in the proposed stormwater network.

Basin "OH" (11350.85sf/ 0.260 acres) is comprised of the area south of the proposed access road to the fire station. This area historically flows into the property to the south of lot 2 and no drainage from this area will be from developed areas, only historical flows will be flowing into adjacent site.

Runoff from the of-site basins OS and OH will follow existing flow paths off of the property and will not be captured in storm water network. While runoff from Basins A through G will be routed via overland flows and a network of inlets and private storm sewer system which combined will convey flows to the improved detention pond facility (pond) and ultimately to Fountain Creek. The pond, located in the lowest corner of Lot 1, e.g. the southeast corner, will also provide water quality for the tributary areas as described above. The basins are outlined in on civil sheet C 3.4 which is included in the Appendix.

#### RUNOFF AND DETENTION

Lot 2 is currently undeveloped and Lot 1 is currently developed. Lot 1 does have onsite detention but due to neglect the onsite detention is no longer functional. Lot 1 and 2 will share a revitalized and developed detention facility in the southeast corner of Lot 1.

The detention pond has been designed for the disturbed basin areas as defined above. The pond will receive overland developed flows as well as hydraulically connected flows by a series of 15" and 24" HDPE storm pipes.

The 10-year and 100-year detention pond volumes were calculated with the rational method per the City of Colorado Springs Drainage Criteria Manual. The pond is designed to contain the 100-year volume plus the water quality volume with a minimum of 1-foot of freeboard.

Flows from the 10-year storm event will be captured and conveyed through the proposed storm sewer, grass swales, and outland to the pond. A portion of the flows from the 100-year storm runoff will be captured by the proposed storm sewer system and swales and conveyed to the detention pond. The remainder of the 100-year storm runoff will sheet flow across the site toward the pond and public rights of way.

The outlet structure from the pond is a Type D Outlet and has been designed to restrict the three required release rates with the use of a water quality plate, a 10-year weir and a 100-year orifice plate on the outlet pipe with an overtopping grate. The allowable release rates have been computed per El Paso County standards and are 2.77 cfs for the 10-year event and 5.29 cfs for the 100-year event.

The emergency spillway for the pond is an engineered berm on the west side of the pond, see plans for dimensions and elevations. The berm will allow water to safely sheet flow at a low velocity to Fountain Creek. The spillway for the pond has been designed with a 1'-0" freeboard and will carry at least the flows for the 100-year storm event.

Some of the storm flows entering the detention pond will be conveyed via a hydraulic system consisting of 15" and 24" HDPE pipe. The flows entering via the storm sewer pipe will be controlled by an energy

![](_page_21_Picture_15.jpeg)

dissipating structure, prior to entering the pond. This structure has been designed to accommodate the 100-year storm flows. Refer to drawings for details.

#### CONCLUSIONS

The majority of the proposed development flows will be routed to the onsite detention and water quality pond. The proposed storm system and detention pond release rates are in conformed with El Paso requirements. Calculations and other reference materials used are attached in the Appendix. The referenced Developed Drainage Map, Figure 1, depicts the drainage design points, developed runoff sub-basins, and configuration of the proposed storm drainage system. The recommendations of this report are in conformance with El Paso County, Colorado.

Proper detention and drainage facilities are proposed to adequately handle all on-site drainage while enhancing the stormwater quality. There will not be any negative impacts on adjacent, upstream, and downstream properties under both existing and future build-out conditions of this site.

![](_page_22_Picture_6.jpeg)

#### REFERENCES

1. City of Colorado Springs Drainage Criteria Manual, 2014 edition.

### APPENDIX A – VICINITY MAP

![](_page_24_Picture_3.jpeg)

Figure 1: Vicinity Map

![](_page_24_Picture_5.jpeg)

### APPENDIX B – CALCULATIONS

![](_page_25_Figure_3.jpeg)

Figure 2: 10-Year Rainfall Depth

![](_page_25_Figure_5.jpeg)

Figure 3: 100-Year Rainfall Depth

![](_page_25_Figure_7.jpeg)

7/16/2018

Precipitation Frequency Data Server

![](_page_26_Picture_4.jpeg)

NOAA Atlas 14, Volume 8, Version 2 Location name: Cascade, Colorado, USA* Latitude: 38,9378°, Longitude: -105,0151° Elevation: 7772.78 ft** * source: ESRI Maps ** source: USGS

![](_page_26_Picture_6.jpeg)

#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular PF_graphical Maps & aerials

#### PF tabular

PDS	DS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹									
Duration		Average recurrence interval (years)								
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.226	0.271	0.350	0.420	0.524	0.610	0.701	0.798	0.934	1.04
	(0.184-0.280)	(0.220-0.336)	(0.283-0.435)	(0.338-0.526)	(0.408-0.693)	(0.460-0.819)	(0.508-0.971)	(0.551-1.15)	(0.617-1.39)	(0.666-1.57)
10-min	0.331	0.397	0.513	0.616	0.768	0.893	1.03	<b>1.17</b>	<b>1.37</b>	1.53
	(0.269-0.410)	(0.323-0.492)	(0.415-0.637)	(0.494-0.770)	(0.597-1.01)	(0.674-1.20)	(0.744-1.42)	(0.807-1.68)	(0.903-2.03)	(0.976-2.30)
15-min	0.404	0.484	0.625	0.751	0.936	1.09	1.25	1.43	<b>1.67</b>	<b>1.86</b>
	(0.328-0.500)	(0.393-0.600)	(0.506-0.777)	(0.603-0.939)	(0.728-1.24)	(0.822-1.46)	(0.907-1.73)	(0.984-2.05)	(1.10-2.48)	(1.19-2.81)
30-min	0.536	0.642	0.828	0.993	<b>1.24</b>	<b>1.44</b>	1.65	1.88	2.20	2.45
	(0.435-0.663)	(0.521-0.795)	(0.669-1.03)	(0.798-1.24)	(0.961-1.63)	(1.09-1.93)	(1.20-2.29)	(1.30-2.69)	(1.45-3.26)	(1.57-3.69)
60-min	0.664	0.781	0.992	1.19	<b>1.48</b>	<b>1.74</b>	2.01	2.30	2.73	<b>3.07</b>
	(0.540-0.822)	(0.634-0.967)	(0.802-1.23)	(0.953-1.48)	(1.16-1.97)	(1.31-2.34)	(1.46-2.79)	(1.59-3.32)	(1.80-4.06)	(1.96-4.63)
2-hr	0.792	0.919	1.16	1.38	<b>1.73</b>	2.03	2.36	2.73	3.26	3.69
	(0.648-0.973)	(0.751-1.13)	(0.941-1.43)	(1.12-1.71)	(1.37-2.29)	(1.55-2.73)	(1.73-3.27)	(1.91-3.91)	(2.18-4.82)	(2.38-5.52)
3-hr	0.885	1.01	1.26	1.50	<b>1.88</b>	2.23	2.61	3.03	3.65	4.17
	(0.727-1.08)	(0.829-1.24)	(1.03-1.54)	(1.22-1.85)	(1.50-2.50)	(1.71-2.99)	(1.93-3.61)	(2.13-4.34)	(2.46-5.40)	(2.70-6.21)
6-hr	<b>1.11</b>	1.25	<b>1.54</b>	1.83	2.31	2.74	3.23	3.77	4.58	5.25
	(0.914-1.34)	(1.03-1.52)	(1.26-1.88)	(1.50-2.24)	(1.86-3.05)	(2.13-3.66)	(2.41-4.44)	(2.68-5.37)	(3.11-6.73)	(3.44-7.76)
12-hr	<b>1.42</b>	1.61	2.00	2.38	3.00	3.56	4.18	4.87	5.88	6.73
	(1.18-1.71)	(1.34-1.94)	(1.66-2.42)	(1.96-2.90)	(2.43-3.93)	(2.78-4.71)	(3.14-5.69)	(3.49-6.87)	(4.04-8.57)	(4.45-9.87)
24-hr	1.75	2.02	2.53	3.03	3.83	4.53	5.30	6.16	<b>7.41</b>	8.45
	(1.47-2.09)	(1.69-2.42)	(2.11-3.04)	(2.51-3.66)	(3.11-4.95)	(3.56-5.93)	(4.01-7.16)	(4.45-8.61)	(5.13-10.7)	(5.64-12.3)
2-day	2.06	2.39	3.02	3.63	4.59	5.43	6.35	7.38	8.88	<b>10.1</b>
	(1.74-2.44)	(2.01-2.84)	(2.54-3.60)	(3.03-4.34)	(3.75-5.88)	(4.30.7.05)	(4.85-8.51)	(5.38-10.2)	(6.20-12.7)	(6.82.14.6)
3-day	2.26	2.61	3.28	3.92	<b>4.94</b>	5.84	6.82	7.92	9.52	<b>10.8</b>
	(1.91-2.67)	(2.21-3.08)	(2.76-3.88)	(3.28-4.67)	(4.06-6.31)	(4.65-7.55)	(5.23-9.10)	(5.81-10.9)	(6.69-13.6)	(7.35-15.6)
4-day	2.43	2.78	3.46	4.12	<b>5.17</b>	6.10	7.11	8.25	9.90	<b>11.3</b>
	(2.06-2.85)	(2.36-3.27)	(2.93-4.09)	(3.46-4.90)	(4.26-6.58)	(4.87-7.85)	(5.47-9.45)	(6.07-11.3)	(6.98-14.1)	(7.67-16.1)
7 <b>-</b> day	2.86	3.23	3.95	4.64	5.74	6.69	7.75	8.92	<b>10.6</b>	12.0
	(2.44-3.34)	(2.76-3.78)	(3.36-4.63)	(3.92-5.48)	(4.75.7.23)	(5.38-8.55)	(6.00-10.2)	(6.61.12.2)	(7.55-15.0)	(8.26-17.1)
10-day	3.27	3.69	4.47	5.20	6.35	7.33	8.40	9.59	11.3	<b>12.7</b>
	(2.80-3.80)	(3.16-4.29)	(3.81-5.22)	(4.41-6.11)	(5.26-7.92)	(5.91-9.29)	(6.53.11.0)	(7.13.13.0)	(8.05-15.8)	(8.75-18.0)
20-day	4.49	5.11	6.16	7.08	8.40	9.48	<b>10.6</b>	<b>11.8</b>	13.4	<b>14.7</b>
	(3.88-5.18)	(4.40-5.90)	(5.29-7.14)	(6.04-8.25)	(6.96-10.3)	(7.66-11.8)	(8.26-13.6)	(8.80-15.7)	(9.62-18.5)	(10.2-20.7)
30-day	5.47	6.24	7.50	8.56	<b>10.0</b>	<b>11.1</b>	12.3	<b>13.4</b>	15.0	16.2
	(4.74.6.28)	(5.40-7.17)	(6.47.8.65)	(7.33-9.92)	(8.29-12.1)	(9.02-13.7)	(9.60-15.6)	(10.1.17.7)	(10.8-20.5)	(11.3-22.6)
45-day	6.63	7.56	9.03	<b>10.2</b>	<b>11.8</b>	<b>13.0</b>	<b>14.1</b>	<b>15.2</b>	<b>16.7</b>	<b>17.7</b>
	(5.77-7.58)	(6.57-8.64)	(7.82-10.4)	(8.79-11.8)	(9.78-14.1)	(10.5-15.8)	(11.1-17.8)	(11.4-19.9)	(12.0-22.6)	(12.5-24.6)
60-day	7.56	8.59	<b>10.2</b>	11.5	<b>13.1</b>	14.3	15.4	16.5	17.8	<b>18.7</b>
	(6.60-8.61)	(7.48-9.78)	(8.85-11.7)	(9.89-13.2)	(10.9.15.5)	(11.6-17.3)	(12.1.19.3)	(12.4-21.5)	(12.9.24.1)	(13.3-26.0)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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#### PF graphical

Figure 4: Design Storm Distribution of 1-Hour NOAA Atlas Depths

Hydrology

![](_page_27_Figure_3.jpeg)

6-52

City of Colorado Springs Drainage Criteria Manual, Volume 1 May 2014

Figure 5: TIF Curve for El Paso County

![](_page_27_Picture_8.jpeg)

Duration (minutes)	5	10	15	30
Ratio to 1-Hr Depth	0.29	0.45	0.57	0.79

#### Adjustment Factors to Obtain N-Minute Estimates From One-Hour Values

#### From NOAA Atlas 2 Vol. III Table 12

One-Hour Design Point Rainfall Values for Various Parts of Western El Paso County/Eastern Teller County

	5-Yr	10-Yr	100-Yr
Cascade	1.05	1.25	2.08
Woodland Park 0.979		1.18	2.04
Green Mountain Falls	1.00	1.20	2.01

![](_page_29_Picture_2.jpeg)

Figure 6: Web Soil Map

#### Pike National Forest, Eastern Part, Colorado, Parts of Douglas, El Paso, Jefferson, and Teller Counties 47-Sphinx, warm-Rock outcrop complex, 15 to 80 percent slopes Map Unit Setting

National map unit symbol: jpjz

National map unit symbol: jpp Elevation: 6,500 to 9,200 feet Mean annual precipitation: 15 to 24 inches Mean annual air temperature: 43 to 48 degrees F Frost-free period: 70 to 125 days Farmland classification: Not prime farmland

#### Map Unit Composition

Sphinx, warm, and similar soils: 60 percent Rock outcrop: 25 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### Description of Sphinx, Warm

Setting

Landform: Mountain slopes Landform position (three-dimensional): Mountaintop, mountainflank Down-slope shape: Linear, convex Across-slope shape: Linear, convex Parent material: Weathered from granite

#### Typical profile

Oi - O to 1 inches: slightly decomposed plant material A - 1 to 5 inches: gravelly coarse sandy loam AC - 5 to 13 inches: very gravelly loamy coarse sand Cr - 13 to 61 inches: weathered bedrock

#### Properties and qualities

Slope: 15 to 70 percent Depth to restrictive feature: 10 to 20 inches to paralithic bedrock Natural drainage class: Somewhat excessively drained Runoff class: Very high Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr) Depth to water table: More than 80 inches Depth to water table: More than 60 incres Frequency of flooding: None Frequency of ponding: None Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Available water storage in profile: Very low (about 0.9 inches) Interpretive groups Land capability classification (irrigated): None specified Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7e Hydrologic Soil Group: D Other vegetative classification: Ponderosa pine/kinnikinnick (PIPO/ARUV) (C1140) Hydric soil rating: No

## Description of Rock Outcrop

Setting

Landform: Mountain slopes Landform position (three-dimensional): Mountaintop, mountainflank Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Jope Jope, enterly contra-Typical profile

R - 0 to 61 inches: bedrock

#### Properties and qualities

Slope: 15 to 80 percent Depth to restrictive feature: 0 inches to lithic bedrock Runoff class: Very high Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr) Available water storage in profile: Very low (about 0.0 inches) Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8 Hydrologic Soil Group: D Hydric soil rating: No

#### Minor Components

Sphinx, dark surface Percent of map unit: 10 percent Landform: Mountain slopes Landform position (three-dimensional): Mountainflank Down-slope shape: Linear, convex Across-slope shape: Linear, convex Other vegetative classification: Ponderosa pine/kinnikinnick (PIPO/ARUV) (C1140) Hydric soil rating: No Garber Percent of map unit: 5 percent Landform: Drainageways, mountain slopes Landform position (three-dimensional): Mountainbase Down-slope shape: Linear, convex, concave Across-slope shape: Linear, convex, concave Hydric soil rating: No

Figure 8: Soil Type 47 Description pt.2

Figure 7: Soil Type 47 Description pt.1

![](_page_29_Picture_30.jpeg)

#### **Calculations for Sizing of Detention Basin**

#### **Composite Runoff Coefficient Calculations**

Composite Runoff coefficients were calculated for each basin using the formula:

$$C_c = \frac{C_1 A_1 + C_2 A_2 + \cdots + C_i A_i}{A_t}$$

Where:

 $C_c$  = composite runoff coefficient of total area

C_i = runoff coefficient for subarea corresponding to surface type of land use

 $A_i$  = area of surface type corresponding to  $C_i$ 

 $A_t$  = total area of all subareas where composite runoff coefficient applies

I = number of surface types in the drainage area

Values for runoff coefficients for different surface types were found in City of Colorado Springs Drainage Criteria Manual Chapter 6, Table 6-6

#### **Ten Year Calculations**

Historic Ten-Year Runoff Coefficient:

Lot 1:

 $C_1 = \frac{0.77*4230sf + 0.92*1420sf + 0.66*12900sf + 0.25*46404sf}{67954sf}$  $C_1 = 0.36$ 

Lot 2:

$$C_{c,1} = \frac{0.25 * 87555 sf}{87555 sf}$$
$$C_{c,1} = 0.25$$

10 Year Runoff Coefficient for Total Historic Site

$$C_T = \frac{0..36*1.56ac + 0.25*2.01ac}{3.57ac}$$
$$C_T = 0.30$$

Developed Ten-Year Runoff Coefficient

Basin A:

$$C_{c,a} = \frac{0.92*13224.93\,sf + 0.25*690.25sf}{13915.18sf}$$

$$C_{c,a}=0.89$$

Basin B:

$$C_{c,b} = \frac{0.77*3381.81sf + 0.92*3152.60sf + 0.66*2605.17sf + 0.25*2669.63}{11748.61sf}$$

$$C_{c,b} = 0.68$$

![](_page_30_Picture_27.jpeg)

Basin C:

$$C_{c,c} = \frac{0.92*3377.09sf + 0.25*5115.90sf}{8492.99sf}$$
$$C_{c,c} = 0.52$$

Basin D:

$$C_{c,d} = \frac{0.92 \times 2507.66sf + 0.25 \times 4903.04sf}{7410.70sf}$$
$$C_{c,d} = 0.48$$

Basin E:

$$C_{c,e} = \frac{0.77*9859.38sf + 0.92*5061.99sf + 0.66*1708.76sf + 0.25*18600.46sf}{5061.99sf}$$

$$C_{c,e} = 0.51$$

Basin F:

$$C_{c,f} = \frac{0.92*3206.43sf + 0.25*18294.91sf}{21500.08sf}$$
$$C_{c,f} = 0.35$$

Basin G:

$$C_{c,g} = \frac{0.77*4230.0sf + 0.92*1820.10sf + 0.66*9199.21sf + 0.25*20617.73sf}{35865.94sf}$$
  
$$C_{c,g} = 0.45$$

Composite 10 Year Runoff Coefficient for Total Developed Site

$$C_T = \frac{0.89*0.319ac + 0.68*0.270ac + 0.52*0.195ac + 0.48*0.170ac + 0.51*0.809ac + 0.35*0.494ac + 0.45*0.823ac}{3.08ac}$$

 $C_{T} = 0.52$ 

#### **100 Year Calculations**

Historic Hundred-Year Runoff Coefficient:

Lot 1:

$$C_1 = \frac{0.83*4230sf + 0.96*1420sf + 0.74*12900sf + 0.50*46404sf}{67954sf}$$
  
$$C_1 = 0.55$$

Lot 2:

$$C_{c,1} = \frac{0.5 \cdot 87555 sf}{87555 sf}$$
$$C_{c,1} = 0.50$$

Runoff Coefficient for Total Historic Site

$$C_T = \frac{0.55*1.56ac + 0.5*2.01ac}{3.57ac}$$
$$C_T = 0.52$$

![](_page_31_Picture_23.jpeg)

Developed Hundred-Year Runoff Coefficient

Basin A:

$$C_{c,a} = \frac{0.96*13224.93 \, sf + 0.5*690.25 sf}{13915.18 sf}$$
$$C_{c,a} = 0.94$$

Basin B:

$$C_{c,b} = \frac{0.83*3381.81sf + 0.96*3152.60sf + 0.74*2605.17sf + 0.5*2669.63}{11748.61sf}$$
  
$$C_{c,b} = 0.78$$

Basin C:

$$C_{c,c} = \frac{0.96*3377.09sf + 0.5*5115.90sf}{8492.99sf}$$
$$C_{c,c} = 0.68$$

Basin D:

$$C_{c,d} = \frac{0.96*2507.66sf + 0.5*4903.04sf}{7410.70sf}$$
$$C_{c,d} = 0.66$$

Basin E:

$$C_{c,e} = \frac{0.83*9859.38sf + 0.96*5061.99sf + 0.74*1708.76sf + 0.5*18600.46sf}{5061.99sf}$$
  
$$C_{c,e} = 0.67$$

Basin F:

$$C_{c,f} = \frac{0.96*3206.43sf + 0.5*18294.91sf}{21500.08sf}$$
$$C_{c,f} = 0.57$$

Basin G:

$$C_{c,g} = \frac{0.83*4230.0sf + 0.96*1820.10sf + 0.74*9199.21sf + 0.5*20617.73sf}{35865.94sf}$$
  
$$C_{c,g} = 0.62$$

Composite 100 Year Runoff Coefficient for Total Developed Site

$$C_T = \frac{0.94*0.319ac + 0.78*0.270ac + 0.68*0.195ac + 0.66*0.170ac + 0.67*0.809ac + 0.57*0.494ac + 0.62*0.823ac}{3.08ac}$$

$$C_T = 0.68$$

![](_page_32_Picture_19.jpeg)

#### **Time of Concentration Calculations**

Time of concentration for historic and developed areas calculated using:

$$t_{c} = t_{i} + t_{t}$$
  

$$t_{i} = \frac{1.87(1.1 - C_{10})\sqrt{L_{o}}}{S^{0.33}} \text{ for 10 year}$$
  

$$t_{i} = \frac{4.43(1.1 - C_{100})\sqrt{L_{o}}}{S^{0.33}} \text{ for 100 year}$$
  

$$t_{t} = \frac{L_{c}}{C_{v}S_{w}^{0.5}}$$

Where:

t_c=time of concentration

t_i=overland flow time

t_t=travel time in ditch, channel, gutter, storm sewer etc.

C_i= Runoff coefficient

 $L_0$ = Length of overland flow

S = average basin slope

C_v= Conveyance coefficient (from Table 6-7 in Colorado Springs DCM)

Historic Time of Concentration of 10 year storm

$$t_{i} = \frac{1.87(1.1 - 0.30)\sqrt{600}}{11^{0.33}} = 16.61 \text{ min}$$
  
$$t_{t} = 0 \text{ min}$$
  
$$t_{c} = 16.60 \text{ min}$$

Developed Time of Concentration for 10 year storm

$$t_i = \frac{1.87(1.1-0.52)\sqrt{325}}{2^{0.33}} = 15.55 \text{ min}$$
  
$$t_t = \frac{600}{15*0.06^{0.5}} = 163.3 \text{ sec} = 2.72 \text{ min}$$
  
$$t_c = 18.27 \text{ min}$$

Historic Time of Concentration of 100 year storm

$$t_i = \frac{4.43(1.1 - 0.52)\sqrt{600}}{11^{0.33}} = 28.32 \text{ min}$$
  
$$t_t = 0 \text{ min}$$
  
$$t_c = 28.32 \text{ min}$$

Developed Time of Concentration for 100 year storm

$$t_i = \frac{4.43(1.1 - 0.68)\sqrt{325}}{2^{0.33}} = 26.62 \ min$$

$$t_t = \frac{600}{15*0.06^{0.5}} = 163.3 \sec = 2.72 \min$$
  
$$t_c = 29.34 \min$$

#### **Calculating WQCV**

The Water Quality Capture Volume (WQCV) was calculated using:

$$WQCV = 0.91I^3 - 1.19I^2 + 0.78I$$

Where:

WQCV = Water Quality Capture Volume(in)

I = Percent Imperviousness of Basin

Calculating Percent Impervious of Total Site was calculated using

$$I_T = \frac{I_1 * A_1 + I_2 * A_2 \dots + I_i * A_i}{A_t}$$

Where:

 $I_T$  = composite percent impervious of total area

I_i = percent impervious for subarea corresponding to surface type of land use

 $A_i$  = area of surface type corresponding to  $I_i$ 

 $A_t$  = total area of all subareas where composite percent impervious applies

I = number of surface types in the drainage area

Percent Imperious of Site

$$I_T = \frac{1.0*33364 + 0.9*1742 + 0.80*13514 + 0.02*106889}{155509}$$

 $I_T = 0.31$ 

Calculating WQCV

 $WQCV = 0.91(0.31)^3 - 1.19(0.31)^2 + 0.78(0.31)$ 

$$WQCV = 0.155 in$$

#### **Calculating Full Spectrum Detention Volume**

 $V_{required} = ((V_{runoff} - V_{discharge}) + V_{Water Quality})*FS$ 

Where

V_{required} is defined as the total required detention volume

 $V_{\text{runoff}}$  is defined as the runoff volume from the site

V_{discharge} is defined as the allowable discharge volume for storm event

V_{Water Quality} is defined as the additional volume required for detention for water quality

FS is the Factor of Safety

#### **Calculating Site Runoff volume**

From the Rational Method the site runoff volume is calculated using:

$$V_{runoff} = C_t I A_T T$$

Where:

 $C_t$  = The runoff coefficient for the developed site

I = Average Rainfall intensity for a duration equal to the time of concentration in in/hr (Determined using NOAA Atlas 14 rainfall intensity chart for site location)

A_T=Drainage basin area (acres)

T = Duration of Design Storm Event(Equal to Time of Concentration for storm event)

Calculating Runoff Volume for 15min 10-year storm

$$V_{runoff} = 0.52 * \frac{3.0 \text{ in}}{hr} * 3.08 \text{ acre} * 0.25 hr * \frac{3600 \text{ sec}}{hr}$$
  
$$V_{runoff} = 4324.32 \text{ cf}$$

Calculating Runoff Volume for 30min 100-year storm

$$V_{runoff} = 0.68 * \frac{3.30 \text{ in}}{hr} * 3.08 \text{ acre} * 0.5 hr * \frac{3600 \text{ sec}}{hr}$$
  
 $V_{runoff} = 12440.76 \text{ cf}$ 

#### **Calculating allowable Discharge Volume**

From Colorado Spring DCM Volume 1 the allowable release rate for a site can be determined from the historic discharge rate of the existing site using the rational method:

$$V_{discharge} = C_t I A_T T$$

Where:

 $C_t$  = The runoff coefficient for the historic site

I = Average Rainfall intensity for a duration equal to the time of concentration in in/hr (Determined using NOAA Atlas 14 rainfall intensity chart for site location)

A_T=Drainage basin area (acres)

T = Duration of Design Storm Event (Equal to Time of Concentration for storm event)

Calculating Discharge Volume for 15min 10-year storm

$$V_{discharge} = 0.30 * \frac{3.0 in}{hr} * 3.08 \ acre * 0.25 hr * \frac{3600 \ sec}{hr}$$
  
 $V_{discharge} = 2494.8 \ cf$ 

Calculating Discharge Volume for 30min 100-year storm

$$V_{discharge} = 0.52 * \frac{3.30 \text{ in}}{hr} * 3.08 \text{ acre} * 0.5hr * \frac{3600 \text{ sec}}{hr}$$
  
$$V_{discharge} = 9513.504 \text{ cf}$$

![](_page_35_Picture_27.jpeg)

#### **Calculating Additional Water Quality Volume**

Additional Storage Volume for proposed detention pond from WQCV is calculated using:

$$V = \frac{WQCV}{12}A$$

Where:

V= Storage Volume (acre-ft)

WQCV = Water Quality Capture Volume (in)

A = Area of site (acre)

Calculating Additional Storage

$$V = \frac{0.155}{12} 3.57$$
  
V = 0.046 acre-ft = 2008.66 cf additional detention volume

#### **Calculating Total Detention Volume**

Total Detention Volume for 10-year event  $V_{required} = ((V_{runoff} - V_{discharge}) + V_{Water Quality})*FS$   $V_{required} = (4324.32 \text{ cf} - 2494.8 \text{ cf} + 2008.66 \text{ cf})*1.25$   $V_{required} = 4797.725 \text{ cf}$ Total Detention Volume for 100-year event  $V_{required} = ((V_{runoff} - V_{discharge}) + V_{Water Quality})*FS$   $V_{required} = (12440.76 \text{ cf} - 9513.504 \text{ cf} + 2008.66 \text{ cf})*1.25$   $V_{required} = 6169.90 \text{ cf}$ 

![](_page_36_Picture_13.jpeg)

#### **Calculations for Sizing of Pipes**

The proposed sub basins were drawn in such a way that the flows from each basin are captured in one proposed storm inlet as well as use one swale type to convey the flows. This allowed for simple calculations of stormwater pipe sizing and swale sizing.

#### Stormwater Pipe Sizing

Stormwater pipes were designed to contain the maximum expected flows of each basin with some design considerations:

- Maximum discharge of each pipe shall not exceed maximum expected flows
- Depth of flow in pipe is less than half of pipe diameter
- Minimum velocity of 3ft/s and a maximum velocity of 18ft/s
- Minimum slope of 0.5 percent
- Minimum pipe size of 15" diameter

With these considerations in mind a pipe diameter and maximum flow depth were assumed and then the discharge was calculated. If the calculated discharge equaled the maximum expected flow and all requirements were achieve, the pipe was determined to be acceptable. The maximum expected flow for each basin was determined using the rational method and the maximum discharge of each pipe was calculated using the manning equation:

$$Q = \frac{1.49}{n} * A * R^{\frac{2}{3}} * \sqrt{S}$$

Where:

Q is the volumetric flow rate passing through the pipe(ft³/s)

A is the cross-sectional are of the flow normal to the flow direction (ft²)

S is the slope of the pipe in ft/ft

n is the Manning Roughness coefficient (0.012 for Corrugated HDPE Pipe)

R is the hydraulic radius

Calculations for Pipe Sizes by Basin

Basin A

Maximum Expected flow:

$$Q = C_{100} * I * A$$
  

$$Q = 0.94 * \frac{3.3in}{hr} * 0.319 acres$$
  

$$Q = 0.989 cfs$$

Given Slope = 12.9% and in an assumed pipe of 15" diameter

Depth = 2"

V = 9.95 ft/s

A 15" pipe is an adequate as it can convey the required discharge at a flow depth and velocity within standards.

![](_page_37_Picture_27.jpeg)

#### Basin B

Maximum Expected flow:

$$Q = C_{100} * I * A$$
  

$$Q = 0.78 * \frac{3.3in}{hr} * 0.270 acres$$
  

$$Q = 0.695 cfs$$

Given Slope = 4.94% and in an assumed pipe of 15" diameter

Depth = 2.1"

V = 6.29 ft/s

A 15" pipe is an adequate as it can convey the required discharge at a flow depth and velocity within standards.

Basin C

Maximum Expected flow:

$$Q = C_{100} * I * A + Q_B$$
  

$$Q = 0.68 * \frac{3.3in}{hr} * 0.195 \ acres + 0.695 \ cfs$$
  

$$Q = 1.13 \ cfs$$

Given Slope = 2.18% and in an assumed pipe of 15" diameter

Depth = 3.3"

V = 5.53 ft/s

A 15" pipe is an adequate as it can convey the required discharge at a flow depth and velocity within standards.

Basin D

Maximum expected flow:

$$Q = C_{100} * I * A + Q_A + Q_B + Q_C$$
  

$$Q = 0.66 * \frac{3.3in}{hr} * 0.170 \ acres + 0.989 \ cfs + 0.695 \ cfs + 0.44 \ cfs$$
  

$$Q = 2.49 \ cfs$$

Given Slope = 4.79% and in an assumed pipe of 18" diameter

Depth = 3.8"

V = 9.03 ft/s

A 18" pipe is an adequate as it can convey the required discharge at a flow depth and velocity within standards.

Basin E

Maximum expected flow:

 $Q = C_{100} * I * A + Q_A + Q_B + Q_C + Q_D$ 

$$Q = 0.67 * \frac{3.3in}{hr} * 0.809 \ acres + 0.989 \ cfs + 0.695 \ cfs + 0.44 \ cfs + 0.37 \ cfs$$
$$Q = 4.28 \ cfs$$

Given Slope = 8.62% and in an assumed pipe of 24" diameter

Depth = 3.97"

V = 12.60 ft/s

A 24" pipe is an adequate as it can convey the required discharge at a flow depth and velocity within standards.

Basin F

Maximum expected flow:

$$Q = C_{100} * I * A + Q_A + Q_B + Q_C + Q_D + Q_E$$
  

$$Q = 0.57 * \frac{3.3in}{hr} * 0.494 \ acres + 0.989 \ cfs + 0.695 \ cfs + 0.44 \ cfs + 0.37 \ cfs + 1.79 \ cfs$$
  

$$Q = 5.209 \ cfs$$

Given Slope = 16.71% and in an assumed pipe of 24" diameter

Depth = 3.69"

V = 17.01 ft/s

A 24" pipe is an adequate as it can convey the required discharge at a flow depth and velocity within standards.

Basin G

There are no pipes in conjunction with Basin G as all flows are overland sheet flows.

Outflow Pipe Sizing

To size the outflow pipe that conveys water from detention pond to Fountain Creek, the allowable maximum release rate for both the 10 year and 100-year storms were considered as know discharge values and a pipe size and flow depth were determined to match these discharge values

10 Year Outflow

Required discharge of 2.71 cfs and pipe slope of 0.75%

A 24" Pipe would have a discharge of 2.71cfs at a flow depth of approximately 5.75" and a velocity of 4.64 ft/s

100 Year Outflow

Required discharge of 5.29 cfs and a pipe slope of 0.75%

A 24" Pipe would have a discharge of 5.29cfs at a flow depth of approximately 8.16" and a velocity of 5.62 ft/s

![](_page_39_Picture_24.jpeg)

### Appendix C – Details

Refer to Civil Drawing Set

![](_page_41_Picture_0.jpeg)

![](_page_41_Picture_1.jpeg)

### F & D International, LLC Architecture . Engineering Project Management 1930 CENTRAL AVE. SUITE B BOULDER, COLORADO 80302 T : 303.652.3200 WWW. fdFone.com

![](_page_41_Figure_4.jpeg)

## EASEMENTS:

EASEMENTS: UNLESS SHOWN GREATER IN WIDTH OR DESCRIBED HEREIN, SIDE LOT LINES ARE HEREBY PLATTED WITH A FIVE (5) FOOT EASEMENT FOR DRAINAGE AND PUBLIC UTILITIES, THE REAR LOT LINES ARE HEREBY PLATTED WITH A SEVEN (7) FOOT EASEMENT FOR DRAINAGE AND PUBLIC UTILITIES ONLY, AND THE FRONT LOT LINES ARE HEREBY PLATTED WITH A TEN (10) FOOT EASEMENT FOR DRAINAGE AND PUBLIC UTILITIES ONLY WITH THE SOLE RÉSPONSIBILITY FOR MAINTENANCE BEING VESTED WITH THE PROPERTY OWNERS.

A. AN EASEMENT OF (0.196) ACRES +/- FOR DRAINAGE, STORMWATER DETENTION, AND STORMWATER QUALITY FOR THE SHARED USE OF LOT 1, LOT 2 WITH THE SOLE RESPONSIBILITY FOR MAINTENANCE BEING VESTED WITH THE PROPERTY OWNER(S) IS HEREBY PLATTED AS GRAPHICALLY REPRESENTED.

B. A (40) FOOT EXCLUSIVE PUBLIC INGRESS AND EGRESS RIGHT-OF-WAYS FOR THE BENEFIT OF LOTS 1 & 2, AND THE PUBLIC IS HEREBY PLATTED AS SHOWN ACROSS AND OVER LOT 1, GREEN MOUNTAIN FALLS TOWN HALL SUBDIVISION WITH THE SOLE RESPONSIBILITY FOR MAINTENANCE BEING VESTED WITH THE TOWN OF GREEN MOUNTAIN FALLS AS GRAPHICALLY DESCRIBED HEREIN. THIS RIGHT-OF-WAYS SHALL REMAIN AND SHALL NOT BE VACATED OR CHANGED AFTER ANY CONVEYANCE OF LOT 1 TO PRIVATE OWNERSHIP PRIOR TO A RE-PLAT DONE IN FULL COMPLIANCE WITH THE TOWN AND/OR COUNTY SUBDIVISION REGULATIONS.

#### SURVEYOR'S CERTIFICATION

THE UNDERSIGNED LICENSED PROFESSIONAL LAND SURVEYOR IN THE STATE OF COLORADO HEREBY CERTIFIES THAT THE ACCOMPANYING PLAT WAS SURVEYED AND DRAWN UNDER HIS RESPONSIBLE CHARGE AND ACCURATELY SHOWS THE DESCRIBED TRACT OF LAND, AND SUBDIVISION THEREOF, AND THAT THE REQUIREMENTS OF TITLE 38 OF THE COLORADO REVISED STATUTES, 1973, AS AMENDED HAVE BEEN MET BASED ON FACTS KNOWN TO ME. THIS 6TH DAY OF MARCH, 2018.

![](_page_42_Picture_7.jpeg)

WARREN D. WARD, COLORADO PLS 25971

#### PLANNERS CERTIFICATION:

, TODD E. FICKEN, BEING A QUALIFIED PROFESSIONAL ENGINEER, CERTIFY THAT THIS PLAT OF THE AMENDED GREEN MOUNTAIN FALLS FIRE STATION SUBDIVISION HAS BEEN ENGINEERED, DESIGNED AND PLANNED IN ACCORDANCE WITH ALL APPLICABLE DESIGN STANDARDS AND OTHER REQUIREMENTS OF THE TOWN OF GREEN MOUNTAIN FALLS SUBDIVISION REGULATIONS BASED ON FACTS KNOWN TO MF

THIS____ DAY OF _____, 20____.

TODD E. FICKEN, P.E.

![](_page_42_Picture_13.jpeg)

### BE IT KNOWN BY THESE PRESENTS:

THAT THE TOWN OF GREEN MOUNTAIN FALLS IS THE OWNER OF THE FOLLOWING DESCRIBED
LOT 1, GREEN MOUNTAIN FALLS TOWN HALL SUBDIVISION, IN THE TOWN OF GREEN MOUNTAIN FALLS, EL PASO COUNTY, COLORADO, AS SHOWN ON THE SUBDIVISION PLAT RECORDED AT RECEPTION NO.21473433, CONTAINING 1.561 ACRES, $+/-$ .
THAT GREEN MOUNTAIN FALLS-CHIPITA PARK FIRE PROTECTION DISTRICT IS THE OWNER OF THE FOLLOWING DESCRIBED TRACT OF LAND, TO WIT:
LOT 2A, GREEN MOUNTAIN FALLS FIRE STATION SUBDIVISION, IN THE TOWN OF GREEN MOUNTAIN FALLS, EL PASO COUNTY, COLORADO, AS SHOWN ON THE SUBDIVISION PLAT AT RECEPTION NO. 214713433, CONTAINING 1.00 ACRES $+/-$
AND
LOT 2B, GREEN MOUNTAIN FALLS FIRE STATION SUBDIVISION, IN THE TOWN OF GREEN MOUNTAIN FALLS, EL PASO COUNTY, COLORADO, AS SHOWN ON THE SUBDIVISION PLAT AT RECEPTION NO. 214713433, CONTAINING 1.00 ACRES $+/-$
DEDICATION:

THE UNDERSIGNED PARTY IN INTEREST HAS CAUSED SAID TRACT TO BE SURVEYED AND PLATTED INTO LOTS. EASEMENTS AND RIGHT OF WAY AS SHOWN ON THIS PLAT, WHICH PLAT IS DRAWN TO A FIXED SCALE AS INDICATED HEREIN AND ACCURATELY SETS FORTH THE BOUNDARIES AND DIMENSIONS OF SAID TRACT AND THE LOCATION OF SAID EASEMENTS, AND WHICH PLAT SO PLATTED SHALL BE KNOWN AS "THE AMENDED GREEN MOUNTAIN FALLS FIRE STATION SUBDIVISION", GREEN MOUNTAIN FALLS, EL PASO COUNTY, COLORADO.

#### LEGAL DESCRIPTION:

TO WIT A PARCEL OF LAND LOCATED IN THE NORTHWEST QUARTER OF THE NORTHEAST QUARTER OF SECTION 30, TOWNSHIP 13 SOUTH, RANGE 68 WEST OF THE 6TH PRINCIPAL MERIDIAN, COUNTY EL PASO, STATE OF COLORADO DESCRIBED AS FOLLOWS: BEGINNING AT PLS MONUMENT 28685 IN THE SOUTHWEST CORNER OF LOT 2, AMENDED GREEN MOUNTAIN FALLS FIRE STATION SUBDIVISION (1) THENCE SOUTH 77°55'01" EAST, A DISTANCE OF 284.87 FEET; (2) THENCE NORTH 00°58'06" EAST, A DISTANCE OF 260.58 FEET; (3) THENCE NORTH 51°54'57" WEST, A DISTANCE OF 216.33 FEET; (4) THENCE SOUTH 82°10'54" WEST, A DISTANCE OF 120.25 FEET; 5) THENCE SOUTH 81°59'59" WEST. A DISTANCE OF 177.24 FEET: (6) THENCE SOUTH 08°00'33" EAST, A DISTANCE OF 85.96 FEET; 7) THENCE SOUTH 30°35'18" WEST, A DISTANCE OF 62.03 FEET; (8) THENCE NORTH 62"19'11" WEST, A DISTANCE OF 110.52 FEET; (9) THENCE SOUTH 08°01'00" WEST, A DISTANCE OF 143.99 FEET; (10) THENCE ALONG THE ARC OF A NON-TANGENT CURVE TO THE RIGHT HAVING A CENTRAL ANGLE OF 00°20'03", A RADIUS OF 677.53' FEET, AN ARCH LENGTH OF 3.95 FEET AND A CHORD THAT BEARS SOUTH 07'22'46" EAST A DISTANCE OF 3.95 FEET; (11) THENCE SOUTH 77'55'33" EAST, A DISTANCE OF 285.15 FEET TO THE POINT OF BEGINNING: CONTAINING 3.569 ACRES +/-

#### IN WITNESS WHEREOF:

_____

THE AFOREMENTIONED GREEN MOUNTAIN FALLS - CHIPITA PARK FIRE PROTECTION DISTRICT HAS EXECUTED THIS INSTRUMENT THIS _____ DAY OF _____, 2018

RICHARD BOWMAN, BOARD PRESIDENT GREEN MOUNTAIN FALLS - CHIPITA PARK FIRE PROTECTION DISTRICT

ATTEST:

JEFF IDELMAN, BOARD SECRETARY GREEN MOUNTAIN FALLS - CHIPITA PARK FIRE PROTECTION DISTRICT

PLANNING COMMISSION APPROVAL: APPROVED BY THE PLANNING COMMISSION OF THE TOWN OF GREEN MOUNTAIN FALLS, COLORADO, THIS ____ DAY OF _____, 20_____.

CHAIRMAN PLANNING COMMISSION

____ ____

ATTEST: _____ TOWN CLERK

### TOWN COUNCIL APPROVAL:

THE UNDERSIGNED HEREBY APPROVE FOR FILING THE ACCOMPANYING PLAT OF THE "GREEN MOUNTAIN FALLS FIRE STATION SUBDIVISION".

MAYOR

ATTEST_____ TOWN CLERK

### RECORDING STATE OF COLORADO)

COUNTY OF EL PASO) SS

I HEREBY CERTIFY THAT THIS INSTRUMENT WAS FILED FOR RECORD AT MY OFFICE AT ____ O'CLOCK ______ M, THIS _____ DAY OF ______, 20____, AND IS DULY RECORDED AT RECEPTION NO.

COUNTY CLERK AND RECORDER

FEE: _____ SURCHARGE: _____

![](_page_43_Figure_0.jpeg)

NE CORNER

NW1/4NE1/4

SEC. 8 T13S

N00°56'59"E

734.55'

# LEGEND:

- FOUND PLASTIC CAPPED REBAR STAMPED PLS 26965, APPARENT ORIGINAL MONUMENT
- $\bigcirc$  Found aluminum capped rebar stamped PLS 28658, APPARENT ORIGINAL MONUMNET
- (5) FOUND1/2" REBAR, APPARENT ORIGINAL MONUMENT
- SET ALUMINUM CAPPED, 1/2" REBAR STAMPED PLS 25971
- FOUND ALUMINUM CAPPED REBAR, ILLEGIBLE, POSITIONED AS PER MONUMENT RECORDS

CURVE TABLE					
CURVE	LENGTH	RADIUS	BEARING	CHORD	
C1	11.48	17.00	N63°02'43"E	11.27	
C2	45.26	67.00	N63°02'43"E	44.40	
C3	24.99	37.00	N63°02'43"E	24.52	
C4	31.75	47.00	N63°02'43"E	31.15	
C5	38.50	57.00	N63°02'43"E	37.77	
C6	18.24	27.00	N63°02'43"E	17.89	

LINE TABLE				
LINE	LENGTH	BEARING		
L1	84.73	S07°58'34"E		
L2	20.00	S07°58'34"E		
L3	20.14	S07°58'34"E		
L4	87.00	S07°58'34"E		
L5	83.61	S82°23'44"W		
L6	53.38	S43°41'41"W		
L7	127.70	S82°23'44"W		
L8	40.00	S08°01'25"E		
L9	39.41	S08°01'00"E		
L10	115.01	N82°23'44"E		
L11	53.38	N43°41'41"E		
L12	83.87	N82°29'26"E		
L13	15.01	S12°04'29"W		

PROPERTY LINE